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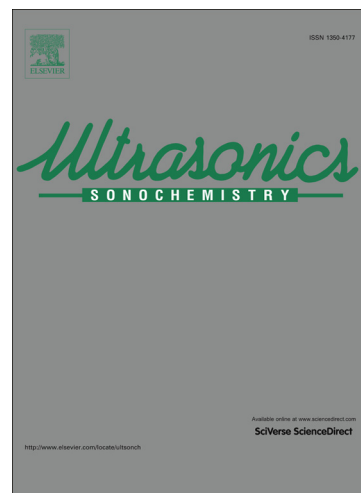
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1 **Design parameters for the separation of fat from natural whole milk**
2 **in an ultrasonic litre-scale vessel**

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13 Keywords: ultrasound processing; ultrasound separation; dairy processing; natural whole milk; milk
14 fat globules

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Abstract

23

24 The separation of milk fat from natural whole milk has been achieved by applying ultrasonic standing
25 waves (1 MHz and/or 2 MHz) in a litre-scale (5 L capacity) batch system. Various design parameters
26 were tested such as power input level, process time, specific energy, transducer-reflector distance
27 and the use of single and dual transducer set-ups. It was found that the efficacy of the treatment
28 depended on the specific energy density input into the system. In this case, a plateau in fat
29 concentration of ~20 % w/v was achieved in the creamed top layer after applying a minimum
30 specific energy of 200 kJ/kg. In addition, the fat separation was enhanced by reducing the transducer
31 reflector distance in the vessel, operating two transducers in a parallel set-up, or by increasing the
32 duration of insonation, resulting in skimmed milk with a fat concentration as low as 1.7 % (w/v) with
33 respect to the unprocessed raw milk after 20 minutes insonation. Dual mode operation with both
34 transducers in parallel as close as 30 mm apart resulted in the fastest creaming and skimming in this
35 study at ~1.6 g fat/min.

36 Keywords: ultrasound processing; ultrasound separation; dairy processing; raw milk; milk fat
37 globules

38

39 1. Introduction

40

41 A technique using ultrasound waves to initiate separation of fat globules from a recombined milk-fat
42 emulsion has been recently reported by Juliano et al.[1, 2] Milk fat globules move to the pressure
43 anti-nodes, due to a time-averaged primary radiation force described, for instance, in Yosioka and
44 Kawasima[3]. Enhanced flocculation (reversible combination) or coalescence (irreversible
45 combination) of the fat droplets may occur at these sites. This increases the effective floccule size of
46 the fat globules, and cause a faster rise velocity and hence separation speed[4].

47 Enhanced creaming of re-emulsified fat orders of magnitude faster relative to natural buoyancy was
48 reported on a litre-scale[1]. On a micro-scale, Grenvall et al.[5] and Johansson et al.[6] showed that
49 acoustic waves could be used to specifically remove fat globules from skim-milk. To the best of our
50 knowledge, no study has yet reported the use of ultrasound to achieve enhanced separation of fat
51 globules from 'natural' whole milk, with particle size distributions and interfacial properties typical
52 of the native product on a litre-scale.

53 Successful trials using natural whole milk have notably only been reported in smaller-scale
54 experiments[2]. Trials using the same parameters as those reported by Juliano et al.[1] to separate
55 fat from natural whole milk on a litre-scale were unsuccessful (data reported in Thesis by Sandra
56 Temmel, University of Erlangen [7]).

57 The reason for this is because the model emulsion system investigated by Juliano et al.[1] and
58 natural whole milk are fundamentally very different. Firstly, the particle size distribution of the
59 recombined milk emulsion used by Juliano et al.[1] is significantly different to those found in natural
60 milk. The volume weighted mean diameter, $D_{[4,3]}$, of the initial emulsions used by Juliano et al.
61 were reported to be 23 μm . This is significantly larger than those used found in 'natural' milk, which
62 are typically between 3-4 μm [4]. There are also a significant number of globules in the size range of
63 10-30 μm found in the recombined emulsions studied (see Fig.2 from Juliano et al.[1]). As noted by
64 Mulder and Walstra[4], even a small number of 'large-globules' present in milk, can make up about
65 2-3 % of the total fat of the milk sample. Because the occurrence of these large globules in the
66 recombined milk emulsion used by Juliano et al. is high, there is a skew of the percentage of total fat
67 that is represented by large globules in the model system.[1]

68 In ultrasound separation, the size of the globules plays a significant role in how easily they can be
69 manipulated by the applied ultrasound and also how strongly they are influenced by
70 sedimentation/buoyancy. The primary radiation force scales with the radius to the third power[3].

71 This means that a globule with a radius of 10 μm is approximately 125 times more strongly
72 influenced by the ultrasound than a globule that is 2 μm in radius. Since a high proportion of the fat
73 is represented by these larger globules, the recombined milk emulsion as studied by Juliano et al.[1]
74 is significantly easier to separate with ultrasound than 'natural' whole milk.

75 Secondly, the interfacial surface properties of the recombined milk emulsions and 'natural' milk, are
76 completely different. In 'natural' milk, the fat globules are stabilised by a complex membrane layer
77 consisting of primarily a tri-layer of phospholipids and proteins[4]. The nature of this surface
78 prevents coalescence from readily occurring. By contrast, a 'recombined' milk emulsion does not
79 have such a stabilising barrier. Instead, it is surrounded by casein micelles and other milk proteins
80 that self-assemble on the surface[8]. Evidence of significant coalescence was observed upon
81 application of ultrasound in the study by Juliano et al. using the recombined milk emulsion. It is
82 uncertain if coalescence will occur readily in 'natural' milk systems when using high frequency
83 ultrasound for the purpose of separation, but its absence would mean that rapid separation would
84 be more difficult to achieve.

85 Further intensification of the process is necessary to achieve separation in 'natural' milk systems.
86 Hence, this present study aims to establish the parameters that are suitable for separation of
87 'natural' whole milk on a litre-scale. Such a study could have significant practical relevance to the
88 dairy industry.

89 An obvious strategy to speeding up the fat separation rate is to increase the acoustic power input or
90 the frequency. According to the primary radiation force described in [3], this would result in a
91 stronger acoustic force and likely result in more effective fat separation. However, it has been
92 previously noted that achieving effective separation is not so simple as increasing the power,
93 because effects such as acoustic streaming must also be considered[9]. Strong streaming velocities
94 may disrupt the separation effectiveness by preventing globules from collecting at the pressure anti-
95 nodes.

96 This current study investigates the efficacy of intensifying the specific energy density on the
97 separation of fat from 'natural' milk systems by modifying the vessel geometry, the use of different
98 frequency operation modes and adjusting the duration of ultrasonic insonation.

99 **2. Materials and Methods**

100 **2.1. Ultrasonic separation trials**

101

102 Raw whole bovine milk was sourced directly from the farm (Department of Primary Industries
103 Ellinbank, Australia) and used for separation tests within 24 hours of obtainment. Milk was
104 maintained at refrigerated temperatures during transportation and was stored in a cool-room at
105 approximately 4 °C prior to usage. All trials were performed with reference to an initial starting
106 sample obtained on the day and trials were performed on several days to mitigate the influence of
107 compositional variation. Gentle mixing by stirring was utilised to recombine any natural cream that
108 may have occurred prior to ultrasound processing.

109 Fully-submersible plate transducers (Sonosys Ultraschallsysteme GmbH, Neuenburg, Germany) of
110 nominal frequency 1 MHz and 2 MHz were available for the separation trials. These transducers are
111 identical in geometry, with dimensions of 160 mm x 160 mm x 30 mm, with an active area of 100
112 mm x 100 mm. A rectangular reaction vessel (width 201 mm, height 180 mm, length variable,
113 constructed from polycarbonate with a wall thickness of 11.9 mm) was used. The two Sonosys
114 transducers were positioned in parallel, as depicted in Figure 1. The plates themselves acted as the
115 reflector in these trials. A 3.2 mm thick stainless-steel plate was positioned on the rear of the
116 transducer on the liquid side of the vessel to prevent seepage of processed product from within the
117 active side to the non-active side of the container, and vice versa.

118 For single-plate operation, one plate is operated while the other plate acts as the reflector. For dual-
119 plate operation, both plates are switched on simultaneously. Since only one 1 MHz and one 2 MHz
120 transducer were available, dual-frequency experiments applied greater power to the system as well
121 as applying two frequencies simultaneously.

122 Milk samples (initial volume 1.6 L) were insonated at 100% nominal power using 1 MHz single (330
123 W), 2 MHz single (290 W) and 1 and 2 MHz in the dual frequency operation mode (620W). The
124 duration of insonation was varied, with settings of 0, 5, 10, 15 and 20 minutes to evaluate the
125 separation with time (processing was stopped for ~3 minutes to collect samples of ~20 mL by pipette
126 from top and bottom at these times). The vessel geometry here was kept constant with a 45 mm
127 sound source to reflector distance, with height and width of the milk in the vessel of 180 mm and
128 201 mm respectively.

129 The effect of vessel geometry was investigated by reducing or increasing the sound source to the
130 reflector distance, while keeping the height and width of the vessel fixed. The distances considered
131 were 30, 45, 85 and 135 mm (alignment accurate to ± 3 mm), corresponding to an initial volume of
132 milk to be processed in the vessel of 1.1, 1.6, 3.1 and 4.9 litres respectively. The operation was with

133 dual-transducers for all the geometries considered here, whilst the 1 MHz single transducer and the
134 2 MHz single transducer was operated only for the 2 smallest geometries.

135 The influence of the power input was further investigated by reducing the nominal power to the
136 transducer to 50 % (179 W) and 25 % (93 W) using the 1 MHz single transducer with the vessel
137 geometry fixed at a distance of 45 mm.

138 Selected trials were repeated under identical processing conditions on different days. The results
139 with the closest matching initial fat concentrations are shown.

140 **2.2. Sample characterization**

141 Samples were collected from near the bottom and top of the separation vessel using a 10 mL
142 serological pipette. For the top layer, care was taken to extract the sample only from a very thin
143 layer (approximately 2-3 mm depth) from the surface of the container. Approximately 20 mL of
144 sample is collected from top and bottom after the prescribed treatment time.

145 **2.2.1. Fat content**

146 Fat content was analysed using the standard Rose-Gottlieb Method[10] to determine the fat
147 concentration of the milk prior to ultrasound processing, and the top and bottom portions after
148 ultrasound application. 10 mL of sample was digested in 2 mL of 25% ammonia solution with 10 mL
149 of ethanol. The fat was then extracted from the mixture using three subsequent extractions with
150 diethyl ether (VWR, AnalaR NORMAPUR) and petroleum ether (VWR, GPR RECTAPUR) into a pre-
151 weighed spherical flask. The solvent was evaporated by rotary evaporation at 60 °C under vacuum
152 (~0.15 atm), dried at 105 °C for 2 hours and left overnight to dry in a dessicator to remove all water
153 content from the sample before weighing.

154 **2.2.2. Particle size**

155 Particle sizing was performed using a Malvern Mastersizer 2000 (Malvern Instruments Ltd.,
156 Worcestershire) with deionised water as the dilutant. A refractive index of 1.46 (with an imaginary
157 refractive index absorbance of 0.001 corresponding to an oil-in-water emulsion) was selected.
158 Optical images were captured using a Leica microscope with a 40X objective.

159 **2.2.3. Zeta-potential**

160 A Zetasizer Nano (Malvern Instruments Ltd., Worcestershire) was used to determine the zeta-
161 potential of the milk fat globules. Phosphate buffer (0.1 M) at a pH of 6.8 was used as the dilutant.
162 Milk was diluted approximately 1:1000 and placed inside a disposable polycarbonate cuvette (ATA
163 scientific, DTS1061). Measurements were repeated a minimum of 10 times per run with a minimum

164 of 3 runs. Commercially available homogenized full cream milk (Devondale, Australia) was used as a
165 comparison for fully disrupted milk fat globules.

166

167 **2.3.Vessel characterization**

168 **2.3.1. Power and temperature**

169

170 The nominal power input could be digitally controlled on the Sonosys control unit, ranging from 5 to
171 100% nominal power. The transducers were operated at 100% nominal power (330 W and 290 W
172 for 1 and 2 MHz respectively) unless otherwise specified. The electrical power draw was determined
173 using a power meter. The energy evolved as heat in the processed milk was determined
174 calorimetrically from temperature measurements using $Q = mC_p\Delta T/t$, where C_p is the specific heat
175 capacity for milk, 3.94 kJ/kg.K[11], m the mass in kg, ΔT the temperature change in Kelvin, and t the
176 time in seconds. The loss of energy due to absorption by the reactor walls and loss of heat to the
177 surroundings by convection is not accounted for in this study, which may contribute to an error of
178 >5% in the actual measurements [12].

179 **2.3.2. Sound pressure**

180 Sound pressure levels were determined using a needle hydrophone (model HNC-1000, Onda Corp.,
181 Sunnyvale, USA). The hydrophone was positioned at various locations across the container to
182 measure the maximal pressure in the vessel.

183

184 **3. Results and discussion**

185

186 **3.1.Vessel characterization and determination of fat surface integrity**

187 A typical change in temperature of the milk during processing with ultrasound operated at 100%
188 nominal power and a reflector/sound source distance of 45 mm, is shown below in Figure 2. At these
189 frequencies, the temperature increase can largely be attributed to absorption of the sound waves as
190 it becomes attenuated through the fluid medium and dissipation of heat from the transducer
191 surface[13].

192 Calorimetry calculations were used to ascertain approximately how much of the electrical power
193 delivered to the transducer is dissipated as heat in the processed milk. These results are shown in

194 Table 1. The energy calculations indicate that the energy dissipated as heat in the processed milk
195 using the different modes of operation with either single (1 or 2 MHz frequency) or dual transducers
196 (1 and 2 MHz frequency) are of similar proportion to the energy input from the electrical power
197 draw for a given geometry. The energy efficiency (attributed to heat loss) can be calculated
198 according to Gogate et al.[14] (power dissipated in liquid/electrical power supplied to the system),
199 and ranges between 28-60% for the values in Table 1, depending on the geometry. These efficiencies
200 are within expected levels for ultrasonic transducers operating in bath-type systems[14], indicative
201 of a uniform distribution over a wide area.

202 The use of dual frequency ultrasound may result in complex interactions in the system which are not
203 known or characterized in this present study. Furthermore, the heterogeneity of milk systems which
204 consists of fat droplets distributed in a liquid matrix, may increase the degree of soundwave
205 reflection, refraction and/or absorption[12]. More detailed assessment of the pressure distributions
206 in such systems would assist in the design of more optimal ultrasonic milk separators in future work.

207 We make an assumption that the two imposing frequencies may impose constructively, which is
208 confirmed by the maximum pressures measured in the system with dual frequency that are
209 approximately the sum of the maximum pressures during single plate operation. The 2 MHz
210 transducer has a lower maximum pressure compared with the 1 MHz transducer, and is likely due to
211 differences in the pressure distributions resultant from their operation.

212 It should also be noted that the maximum pressure detected with the hydrophone under these
213 operating conditions appears to be below the transient cavitation threshold predicted by Apfel[15]
214 for water and blood. However, the cavitation that occurs may still disrupt or damage the integrity of
215 the milk fat globules. To confirm the extent of any damage, the apparent zeta-potential of milk (1.6
216 L) that has been insonated for 20 and 40 minutes at 1 MHz (330 W) was measured and compared to
217 unprocessed whole milk and homogenised full cream milk (Fig. 3).

218 The zeta-potential gives an indication to the relative proportion of casein micelles and other milk
219 proteins that are at the surface of the milk fat globule[8]. A fully disrupted globule in the case of
220 homogenised full cream milk, is completely surrounded by casein micelles and other milk proteins.
221 In comparison, a milk fat globule in its 'native' state will be surrounded by a membrane consisting of
222 a phospholipid tri-layer. The two situations give very different zeta-potential values, in this case -
223 11.2 ± 0.2 mV and -16.2 ± 0.5 mV for unprocessed and homogenized milk respectively. The values
224 obtained here for unprocessed and homogenized milks are similar to those reported by Michalski et
225 al.[8] Values in between the two extremities give a relative indication of the amount of damage

226 incurred by the milk fat globules during any form of processing. In this case, the zeta-potential of the
227 ultrasound processed samples show almost no change compared to the 'native' sample, with values
228 of -11.4 ± 0.2 and -11.5 ± 0.7 mV for 1 MHz processing after 20 and 40 minutes respectively,
229 indicating no significant surface damage by the applied ultrasound.

230 Although the physical disruption of the milk fat globules under these conditions is shown to be
231 negligible, the influence of other sonochemical effects on the milk components should also be
232 considered. Studies performed by Villamiel and De Jong[16] and Chandrapala et al.[17] have
233 previously reported the influence of power ultrasound on milk systems and their components,
234 namely the fat globules, proteins and enzymes. Of primary concern is the possible formation of
235 amyloid aggregates from the sonication of protein solutions, as reported by Stathopoulos et al.[18]
236 However, the recent report by Chandrapala et al.[17] could not find evidence of the formation of β -
237 structures indicative of amyloid structures in milk based systems under the influence of high power
238 ultrasound at 20 kHz frequency.

239 It is possible that the input of ultrasound in milk leads to slight denaturation of the proteins, such as
240 casein and whey, due to a combination of sonochemical and thermal effects. However, 'natural' milk
241 has many anti-oxidative components such as casein[19], enzymes, vitamins and lactoferrins that
242 limit the extent of redox reactions that may occur[20]. In any case, the industrial processing of milk
243 typically requires pasteurisation of separated milk at high temperatures such that any denaturation
244 of proteins and other milk components by the ultrasound during separation is likely to be negligible
245 in comparison.

246 **3.2.Characterization of controls and insonated milk**

247

248 Two controls were performed with milk obtained on different days. These controls were set-aside to
249 cream naturally at ambient room conditions, for 15 minutes and 60 minutes respectively. The 15
250 minute and 60 minute controls had an initial fat concentration determined to be 4.2 % w/v and 4.5
251 % w/v respectively, which are within a fat content range expected for raw whole milk[4]. The result
252 for these two controls are shown below in Table 2. No major change in fat content of samples drawn
253 from the top and bottom was observed in either of the control samples when left to cream at room
254 conditions (20 °C) for the specified duration.

255 An untreated sample from the same batch of milk as the 15 minute control was characterised using
256 microscopy (Fig. 4a) and particle sizing (Fig. 4b). A volume from this same batch of milk was

257 insonated in the experimental vessel using the 1 MHz frequency with a sound source to reflector
258 distance of 45 mm and 100 % (310 W) nominal power for 20 minutes.

259 Microscope images and particle size distributions of samples from the separated top and bottom
260 after insonation are also shown in Figure 4a and Figure 4b respectively. No evidence for significant
261 coalescence of fat globules can be deduced from either, suggesting that the mechanism for
262 enhanced separation is primarily due to flocculation of the globules into larger entities that can be
263 redispersed. The expected mechanism for this would be due to *agglutination*[4] possibly caused by
264 milk serum immunoglobulins[21] that precipitate onto the surface of the fat globules. The
265 separation therefore proceeds similarly to natural creaming albeit much more rapidly.

266 The particle size distributions obtained for the milk shows size distributions typical for raw whole
267 milk with a mean diameter in the range of 3 to 4 μm [22]. The distributions of the separated samples
268 also suggest that there is a clear concentrating effect of the larger fat globules in the cream,
269 evidenced by the shift of the curve towards higher particle size (Fig. 4b). Similarly, there is a higher
270 proportion of smaller globules retained in the bottom sample after processing, as these globules are
271 much more difficult to remove by ultrasound as they experience a smaller force according to [3].

272 3.3.Effects of ultrasound on milk fat separation

273 3.3.1. Frequency operation mode

274

275 In Figure 5, the fat concentration of samples obtained from the top and bottom are plotted as a
276 function of the duration of insonation by ultrasound. The results reported here are for a sound-
277 source to reflector distance of 45 mm unless otherwise stated. Error bars associated with the
278 reported fat concentration from these trials are estimated from systematic error propagation caused
279 by the sampling and fat content analysis. The values obtained for the fat content of the top and
280 bottom layers are estimated to have a relative error of 15% and 5% respectively (maximum absolute
281 error estimated to be $\pm 4\%$ w/v). The relative error of 15% attributed to the fat content of the fat-
282 enriched cream layer is an estimate based on the ability to collect sample from the top of the cream
283 layer. Due to rapid separation, the cream layer is not completely homogenous and the collected
284 samples can sometimes be 'diluted' by skim milk that has been entrained with the fat. The bottom
285 sample is assumed to be well-mixed during processing by the fluid motion caused by acoustic
286 streaming.

287 The dual frequency mode causes the most rapid creaming of fat to the top layer of the vessel (Fig.
288 5a), and causes the most effective skimming of fat from the bottom layer (Fig. 5b) owing to the

289 higher power delivery from the use of two transducers (620 W). The depletion rate of fat from the
290 bottom layer is estimated to be ~ 1.6 g fat/min with the dual-transducer operation mode. The 1 MHz
291 single transducer appears to offer slightly faster separation (~ 1.3 g fat/min) at this geometry
292 compared with the 2 MHz single transducer (~ 0.8 g fat/min), although the power draw of the 2 MHz
293 transducer is lower (290 W versus 330 W). The lower electrical power draw of the 2 MHz transducer
294 (Table 1) is confirmed by the temperature evolution of the two single transducers in Figure 2, where
295 the gradient of the fitted line for 1 MHz ($1.2^{\circ}\text{C}/\text{min}$) is higher than for 2 MHz ($0.95^{\circ}\text{C}/\text{min}$).

296 Although there is a steep increase in fat concentration after 10 minutes of insonation using the
297 single 1 MHz and dual 1 and 2 MHz transducers, after 15 minutes of insonation, all three transducer
298 operation modes result in creaming enhancement to the top layer, achieving what appears to be a
299 saturation fat concentration between 15 to 25% (w/v) in a layer approximately 5 to 10 mm thick,
300 which is representative of a thick loose cream layer that is formed rapidly by flocculation[1].

301 The concentration (% w/v) of fat in the top and bottom samples for the different operation modes
302 performed at 45 mm (Fig. 6a) and 30 mm (Fig. 6b) separation distance are also plotted as a function
303 of the specific energy (calculated as the electrical power consumption per kilogram of fluid, kJ/kg).

304 Figure 6 confirms that for 1 and/or 2 MHz frequencies, either choice of frequency, achieves similar
305 creaming and skimming if we normalise the energy input with the volume/mass and time. In this
306 case, the advantage of using dual transducers is that a higher rate of energy can be put into the
307 system for the same equivalent time as a single transducer operated at 100% nominal power. This
308 means that a desired fat concentration in either the bottom layer (skim product) or the top layer
309 (cream product) can be achieved comparatively quicker.

310 The cream formed for the 30 mm separation geometry appears to plateau at a lower fat
311 concentration (approximately 15 % w/v) compared with the 45 mm geometry. However, this top
312 layer fat concentration is reportedly typical for cream formed at conditions that are more optimal
313 for flocculation (pre-heated milks creamed at low temperature[4]). The more rapid flocculation seen
314 here probably results in the cream being more loosely packed with a lower fat content, explaining
315 why the fat concentration of the cream plateaus at approximately 15-20 % w/v rather than 20 – 25
316 % w/v.

317 In the case of the 30 mm geometry, a smaller volume (1.1 L) of milk was processed and beyond 10
318 minutes the temperature of the vessel became high ($> 40^{\circ}\text{C}$). It should be noted that very high
319 temperatures can deactivate the agglutination mechanism that may be responsible for enhanced
320 flocculation due to denaturation of the immunoglobulins present in the milk serum[21]. It is

321 therefore possible that increasing the temperature beyond 40 °C may also reduce the efficacy of the
322 ultrasound. However, this does not appear to be a problem in the current operation of the
323 separation system, as the skimming of the bottom product continues to proceed (Fig. 6b) in spite of
324 the higher temperatures. It has been reported by Caplan et al.[21] that temperatures of 76.9 °C (not
325 reached in this current study) are required to completely deactivate the natural creaming
326 mechanism.

327 It may appear surprising that both 1 and 2 MHz single transducer operations achieve similar fat
328 separation with energy input, even though the higher frequency would be expected to generate a
329 stronger acoustic force according to, for instance, Yosioka and Kawasima[3]. This assumption
330 however would require that the transducers to be geometrically identical in terms of their acoustic
331 field distribution and require the separation to be entirely dependent on the rate at which individual
332 globules are moved to the anti-nodal planes. These are not the case, as evident from the different
333 maximal pressures determined by hydrophone measurement for the 1 and 2 MHz (single-mode)
334 transducers in Table 1.

335 It has been claimed by Whitworth et al.[23] that for acoustic separations where ultrasound-assisted
336 flocculation is the mechanism for faster separation, the rate-determining step is not how quickly the
337 globules/particles will move to a banding location (this is usually in the order of 1-2 seconds[24]),
338 but rather how quickly they flocculate and hence rise/precipitate due to gravity owing to the larger
339 floccule size (usually in the order of tens of seconds to minutes). What this suggests is that when
340 operating on a litre-scale such as that considered here, the influence of the frequency for the
341 separation of fat globules in milk (provided that it is sufficiently high enough to influence the fat
342 globules and is not too high such that it is strongly attenuated in the system) is not as critical as
343 other parameters such as the energy density which influences the number and the intensity of
344 possible collision events in the overall system.

345

346 **3.3.2. Vessel geometry**

347 Using the dual-transducer mode operation, the distance between the 2 plates was varied to 30 mm,
348 45 mm, 85 mm and 135 mm. The influence on the fat content of the collected top and the bottom
349 samples after prescribed durations of insonation can be observed in Figure 7.

350 At the largest geometry investigated (135 mm), the creaming enhancement to the top is the slowest.
351 Another observation for the 135 mm geometry is that the fat depletion in the bottoms does not
352 follow the trend of decreasing fat concentration with time observed for the smaller geometries. A

353 possible explanation for this is that the larger distance between the sound-source and reflector here
354 results in higher intensity acoustic streaming due to more attenuation of the ultrasound over this
355 distance. This can cause high recirculation of separated fat that reduces the efficacy of the
356 separation, similar to observations previously observed in other systems[9].

357 Shortening the distance between the two transducer plates increases the fat separation rate, and it
358 is evident that the separation proceeds most rapidly for the 30 mm plate-to-plate distance. The rate
359 of fat removal from the bottoms is ~ 1.6 g fat/min. As the processed milk volume is reduced with
360 decreasing plate distance, a higher specific energy is input to the system more quickly if the same
361 power draw (620W) is utilized as for the larger volumes. This higher energy density likely enhances
362 the rate at which globules are flocculated by the agglutinin (immunoglobulins located in the milk
363 serum)[21], possibly by enhancement of the number and the intensity of the globule-globule
364 collisions in the system.

365 A plot for a fixed, dual transducer operation set-up with varying vessel geometries is also plotted as
366 a function of specific energy in Figure 8.

367 Figure 8 suggests that for a fixed nominal power input, the process is scalable by geometry within
368 the investigated range. Of course, these results would be specific to this particular system and
369 transducer type used in this present study. Increasing the vessel geometry further may result in less
370 effective separation due to sound attenuation, which we observe in the results for the 135 mm
371 geometry in Figure 7b.

372

373 **3.3.3. Energy input**

374

375 The power delivery to the transducers has been kept thus far at 100% nominal output. For the 1
376 MHz single transducer, the output was now lowered to 50% (179 W) and 25% (93 W) to ascertain
377 the effect of power delivery from a given transducer and geometrical setup. The result for the
378 change in fat concentration of the top layer is plotted in Figure 9 as a function of insonation time.

379 As expected, the lower the power input, the slower the rate at which fat is enriched in the top layer
380 resulting in a lower fat concentration. After 20 minutes insonation, fat content at the top layer was
381 determined to be 5.2 ± 0.8 % w/v, 7.1 ± 1.1 % w/v and 13.5 ± 2.0 % w/v at the 25%, 50% and 100%
382 nominal power levels respectively. This would suggest that there is also scalability of fat separation
383 with regards to power and time for a given geometrical volume and transducer. Similar results for

384 the separation of oil droplets suspended in water have been reported by Nii et al.[25], where the
385 extent of separation was found to be determined by the power input and/or duration of insonation.

386 As shown earlier in Figure 6 and 8, plotting the fat concentration of separated top and bottom layers
387 as a function of the specific energy provides some interesting insight into how to more effectively
388 and efficiently achieve separation. There appears to be a threshold specific energy input at
389 approximately 100 kJ/kg, where significant creaming and separation begins to occur.

390 Also interesting is that above 200 kJ/kg of energy input, the creaming efficacy plateaus for the 30
391 mm and 45 mm geometries considered, suggesting that the saturation concentration of the cream
392 able to be collected after separation by ultrasound is approximately 20-25% w/v, which is the limit
393 for cream layers formed by natural sedimentation[4]. Higher specific energy inputs were not
394 considered with the larger geometries since longer insonation time (>20 minutes) were required.

395 For the 30 mm separation distance, this plateau is somewhat lower at approximately 12-15% w/v.
396 These concentrations are also lower than for cream separated by use of a centrifuge heated to 40 °C,
397 which can usually achieve upwards of 40% w/v[4]. Cream with a fat content higher than 80% can be
398 generated in the production of anhydrous milk fat by centrifugation[22] (typically at temperatures
399 >90°C and g-force > 12000). It should however be noted that in the centrifuge, the cream product is
400 collected from between very narrow regions (ie. between stacked disc plates) that enables high-
401 density crowding of the fat globules. In the ultrasound separator, the cream that is collected is
402 possibly resultant from the rapid formation of irregular large floccules and hence has a lower fat
403 crowding concentration. Further evaluation of the flocculation mechanism of the milk fat globules
404 under the influence of ultrasound is suggested in future work to confirm this.

405 Although the cream formation is limited by a saturation fat content due to the proposed flocculation
406 mechanism, further input of energy causes continued skimming of the bottom fraction indicating
407 that there is continued removal of fat globules from the bulk bottom fraction of the milk by
408 ultrasound. Furthermore, the results suggest scalability with respect to both power and vessel
409 geometry within this investigated parameter space that is simpler than expected. The influence of
410 energy dependent effects such as acoustic streaming must still be considered for larger vessel
411 geometries, and may be the cause of errors in these trials that causes deviation of results from
412 expected trends.

413 **Conclusion**

414

415 It has been demonstrated that fat separation in natural whole milk on a litre scale using ultrasonic
416 standing wave system is possible. Several important parameters have been evaluated to understand
417 their impact on the ultrasound separation efficacy. It was found that a higher energy density was key
418 to increasing the rate of fat separation, and could be achieved by reducing the vessel geometry or
419 using dual transducers. These observations are useful in providing further insight into suitable design
420 parameters for the scale-up of ultrasonic separation vessels.

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426 the analytical techniques performed in this study.

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428

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485

486 **Table captions**

487 Table 1: Determination of energy input to the system from power draw and calorimetry. The
488 pressures reported are the maximum pressure in the system determined using a needle
489 hydrophone.

490 Table 2: Fat content of control samples

491

492 **Figure captions**

493 Figure 1: Schematic of the experimental set-up for batch mode operation for raw milk fat separation.
494 The adjustable distances between the two transducer plates considered in the experiments are 30
495 mm, 45 mm, 85mm and 135 mm.

496 Figure 2: Temperature change in the vessel with application of 1 MHz (330 W), 2 MHz (290 W) and
497 1+2 MHz (620 W) dual frequency with a transducer-reflector distance of 45 mm (processing volume
498 of 1.6 L).

499 Figure 3: Zeta-potential of unprocessed whole milk, ultrasound processed milk and homogenized full
500 cream milk. 1 MHz ultrasound at a nominal power of 330 W was input to a volume of 1.6 L.
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502 Figure 4: a) Microscopy images obtained of i) initial milk sample ii) bottom product after 20 minutes
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506 45 mm sound source to reflector distance.

507 Figure 5: Fat content of the a) top and b) bottom samples for different frequency modes of
508 operation. The transducer-reflector distance is kept constant here at 45 mm. Error bars indicate the
509 relative error attributed to the sampling and fat content analysis.

510 Figure 6: Concentration of fat in the top and bottom for various operating modes of separation for a
511 transducer-reflector separation distance of a) 45 mm and b) 30 mm, plotted as a function of the
512 specific energy density. Error bars indicate the relative error attributed to the sampling and fat
513 content analysis.

514 Figure 7: Change in fat content (% w/v) of the top (a) and bottom (b) portions as a function of
515 insonation time, for several transducer-reflector distances (30 mm, 45 mm, 85 mm and 135 mm)
516 using the dual separation mode. Error bars indicate the relative error attributed to the sampling and
517 fat content analysis.

518 Figure 8: Concentration of fat in the top and bottom for the dual transducer operating mode for
519 various separation distances between reflector and transducer, plotted as a function of the specific
520 energy density. Error bars indicate the relative error attributed to the sampling and fat content
521 analysis.

522 Figure 9: Effect of nominal power delivery to the 1 MHz transducer on the creaming and skimming
523 behaviour using a 45 mm transducer-reflector geometry as a function insonation time. Error bars
524 indicate the relative error attributed to the sampling and fat content analysis.

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Table 1: Determination of energy input to the system from power draw and calorimetry. The pressures reported are the maximum pressure in the system determined using a needle hydrophone.

Separation distance (mm)	Frequency operation mode	Electrical power draw (W)	Calorimetric power (W)	Pressure (kPa)
30	1 MHz	332±7	94±9	86±13
30	2 MHz	288±6	83±8	16±2
30	Dual	620±12	134±13	109±16
45	1 MHz	332±7	138±14	59±9
45	2 MHz	288±6	106±11	20±3
45	Dual	620±12	214±21	80±12
85	Dual	620±12	363±36	75±11

Table 2: Fat content of control samples

Sample	% Fat w/v	% Enhancement (relative to initial)
Initial control 1	4.2±0.2	
15 min control 1 bottom	4.3±0.2	2±0.1
15 min control 1 top	4.3±0.2	2±0.1
Initial control 2	4.5±0.2	
60 min control 2 bottom	4.6±0.2	2±0.1
60 min control 2 top	4.7±0.2	4±0.2

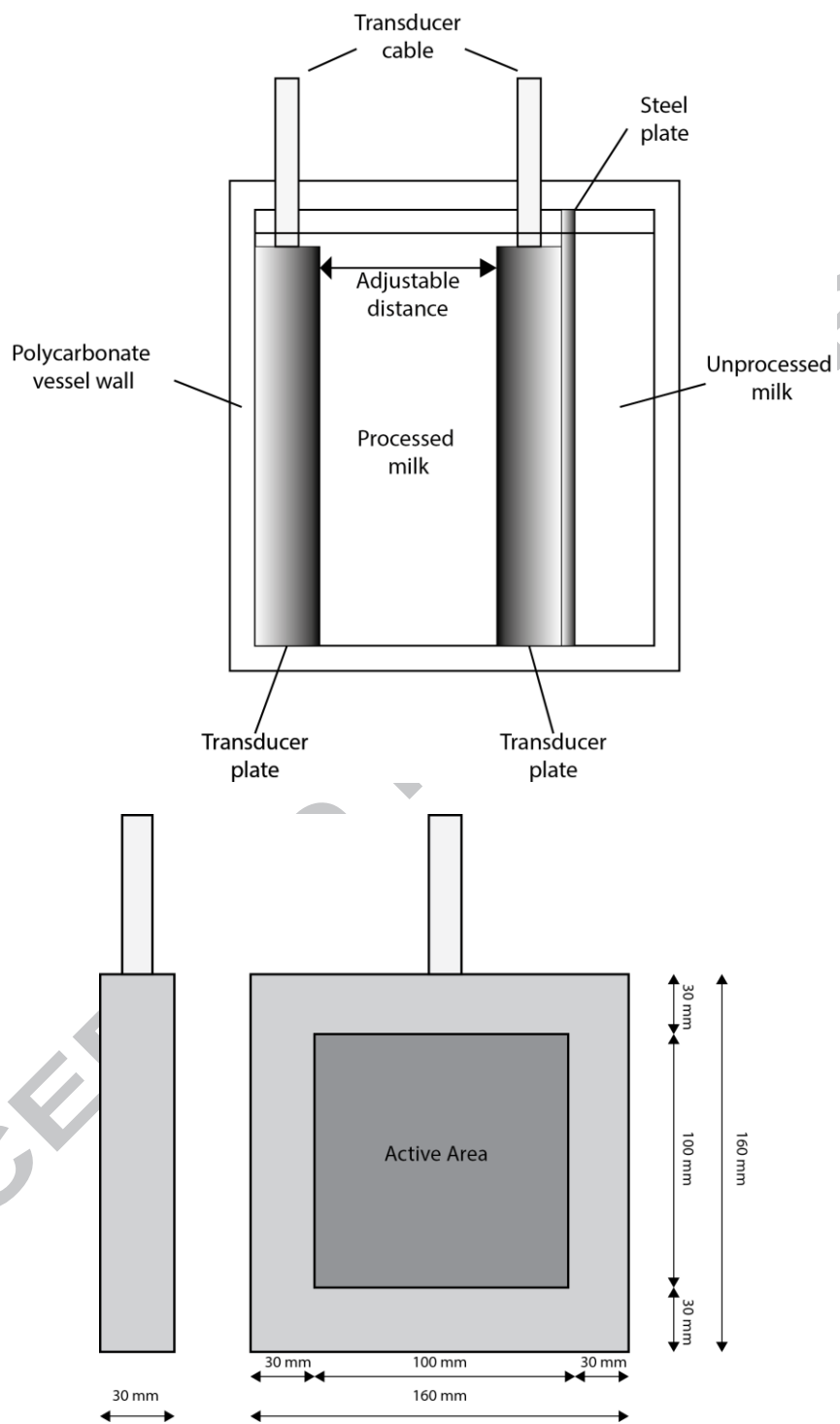


Figure 1: Schematic of the experimental set-up for batch mode operation for raw milk fat separation. The adjustable distances between the two transducer plates considered in the experiments are 30 mm, 45 mm, 85mm and 135 mm.

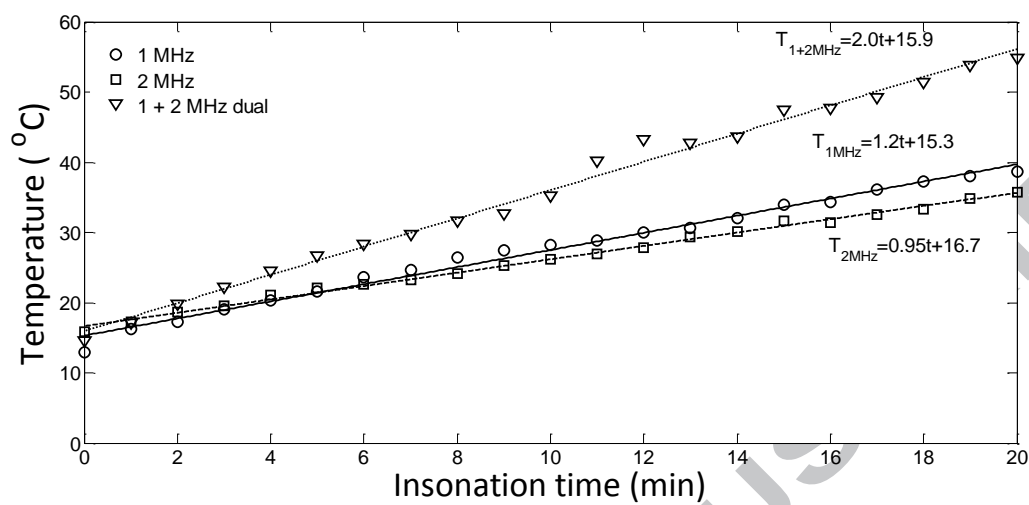


Figure 2: Temperature change in the vessel with application of 1 MHz (330 W), 2 MHz (290 W) and 1+2 MHz (620 W) dual frequency with a transducer-reflector distance of 45 mm (processing volume of 1.6 L).

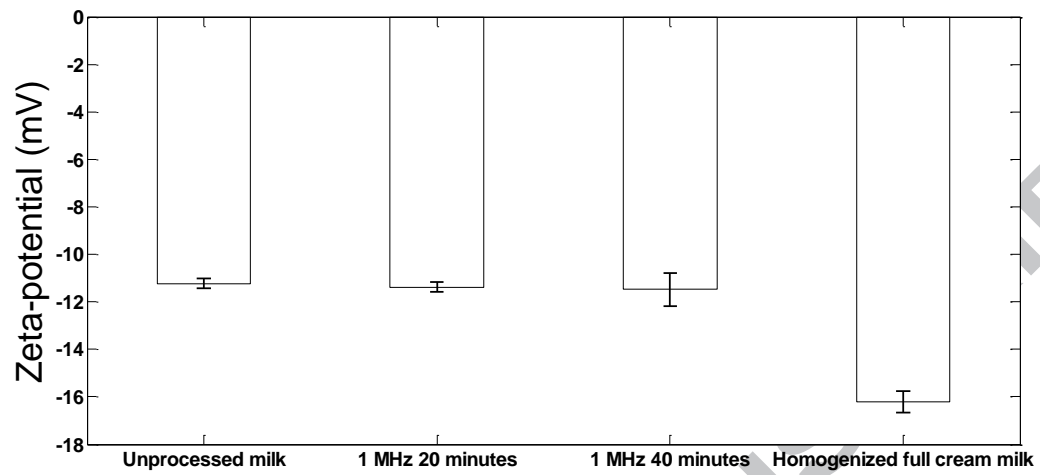
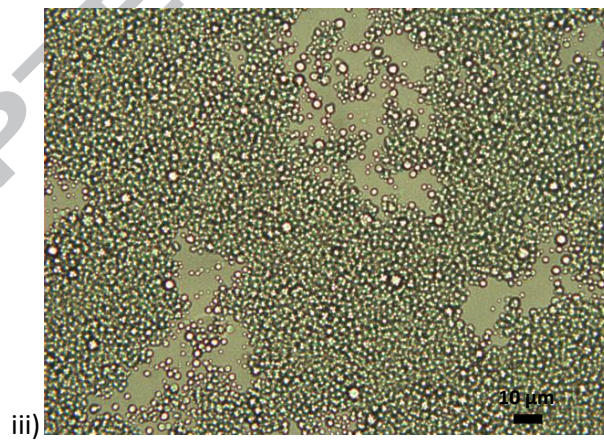
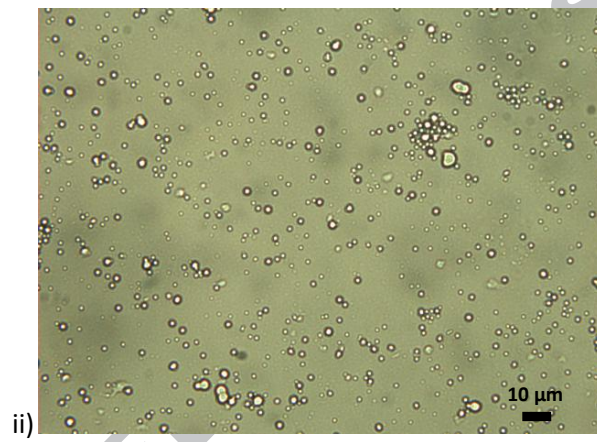
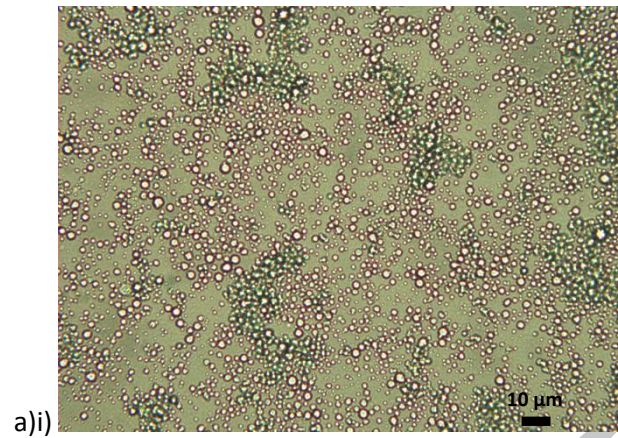


Figure 3: Zeta-potential of unprocessed whole milk, ultrasound processed milk and homogenized full cream milk. 1 MHz ultrasound at a nominal power of 330 W was input to a volume of 1.6 L. Homogenized milk was obtained off the shelf from the supermarket.



b)

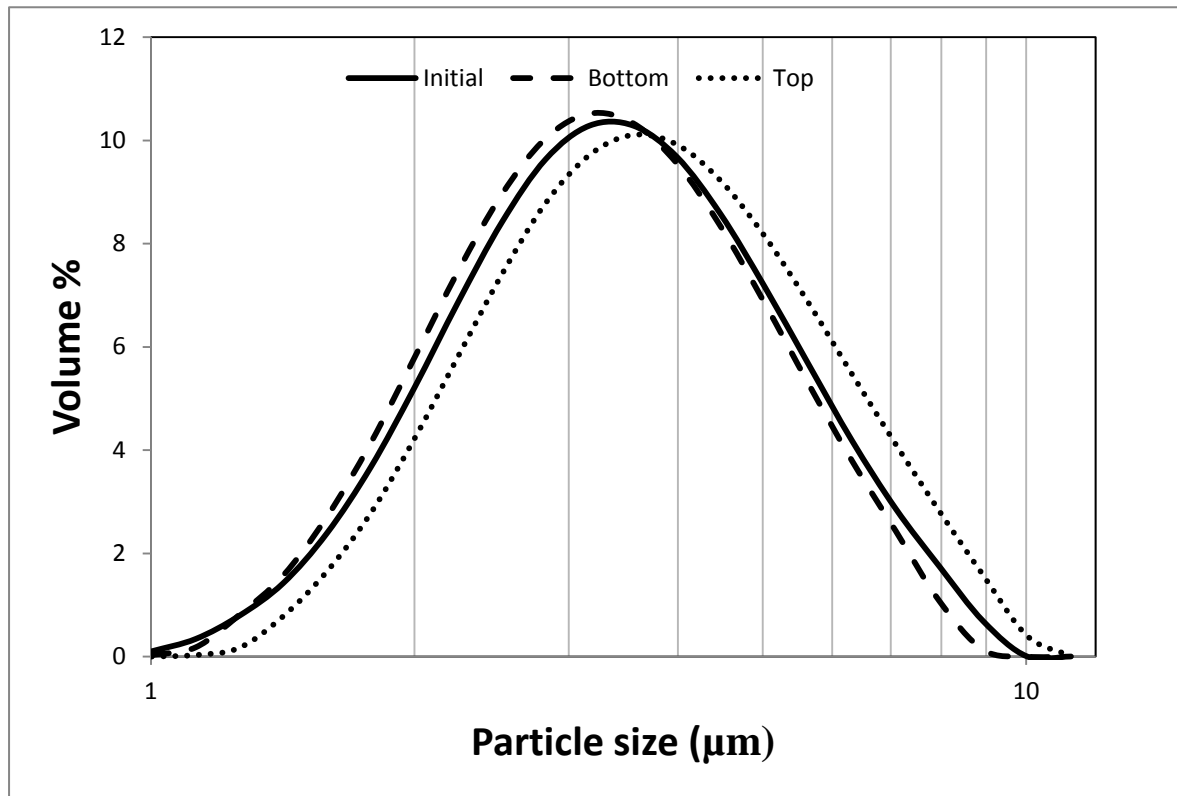


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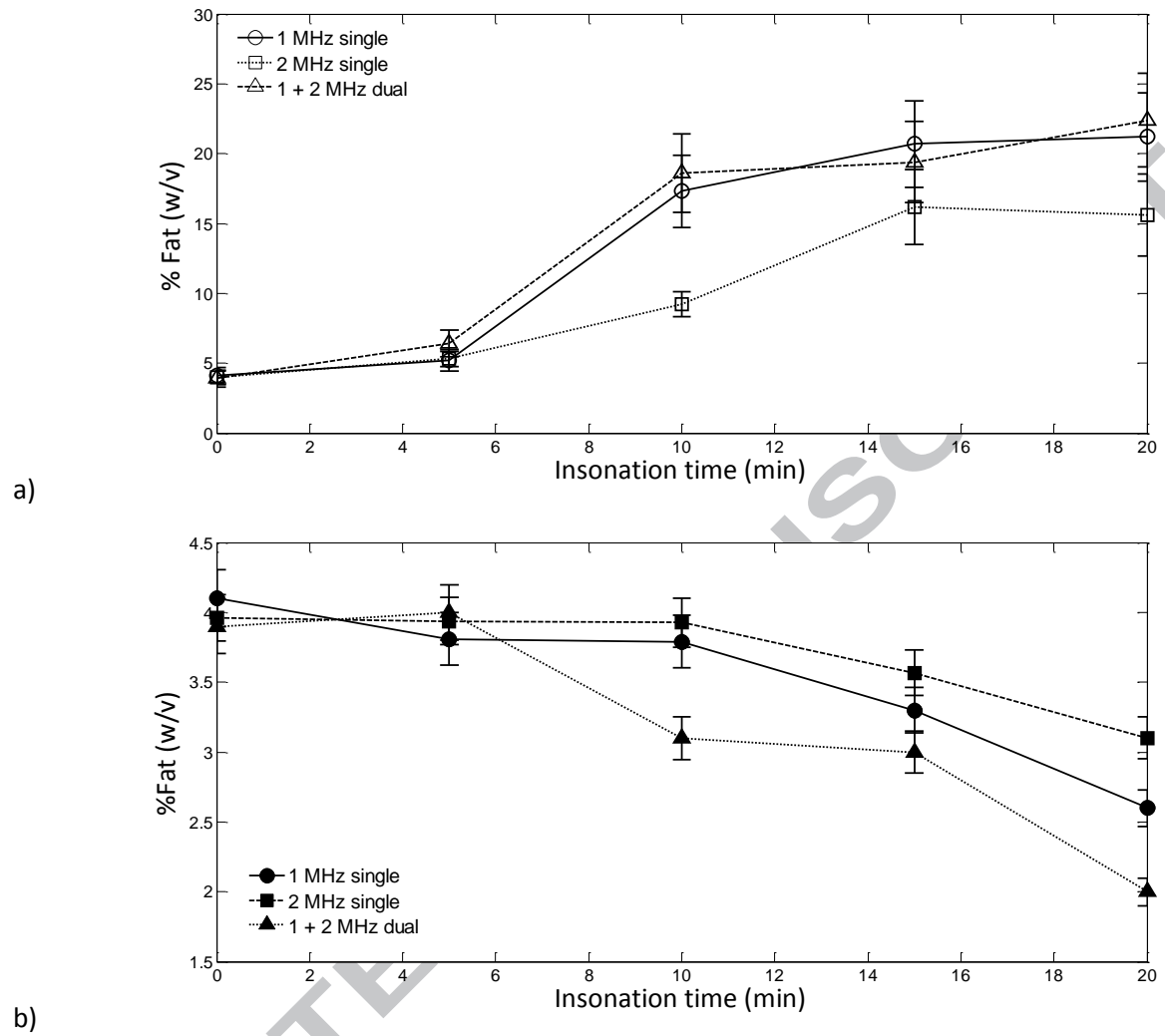
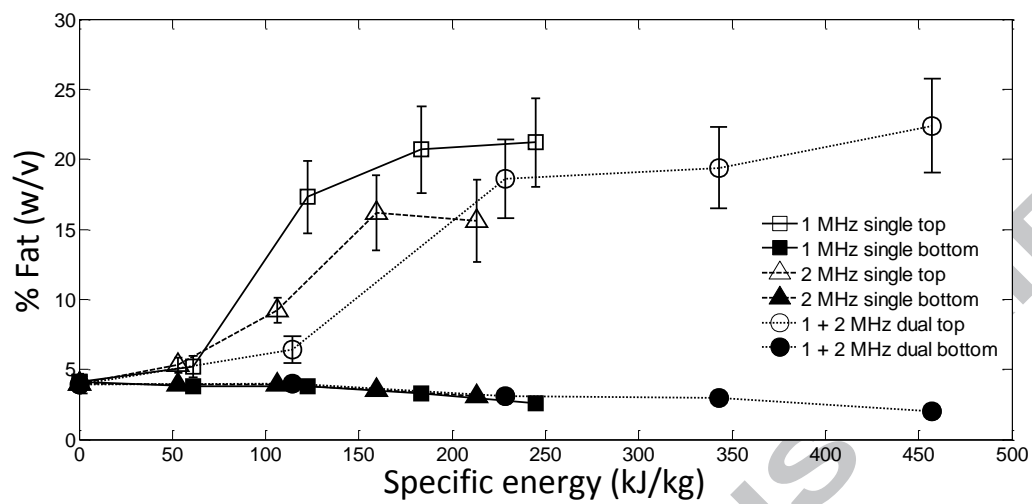


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a)



b)

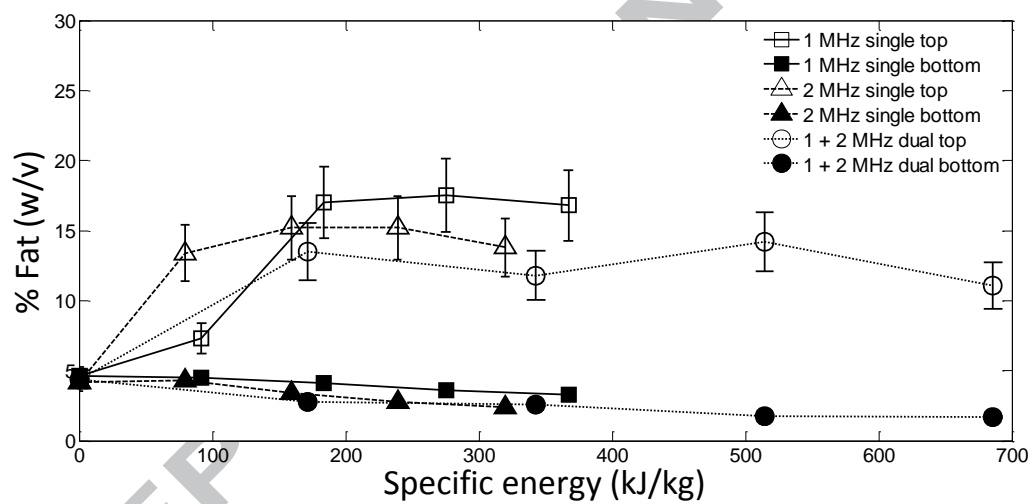
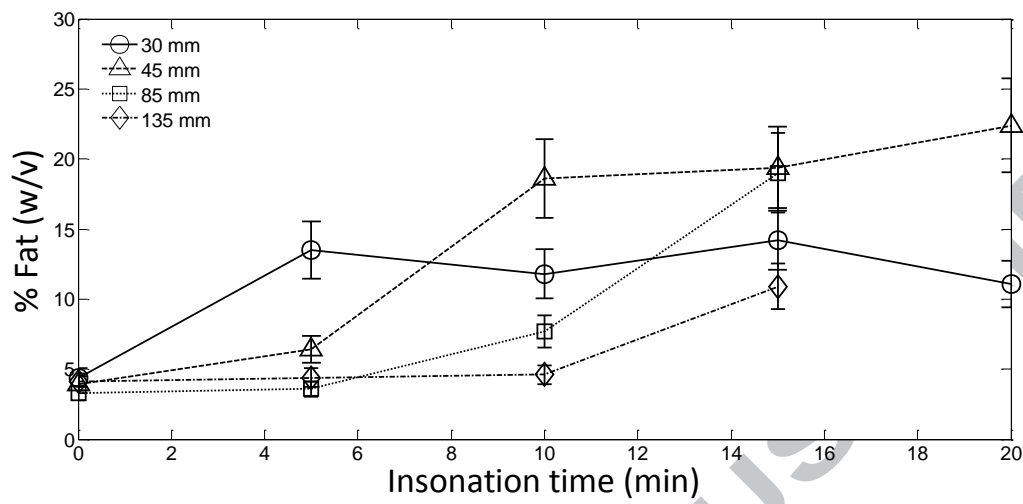


Figure 6: Concentration of fat in the top and bottom for various operating modes of separation for a transducer-reflector separation distance of a) 45 mm and b) 30 mm, plotted as a function of the specific energy density. Error bars indicate the relative error attributed to the sampling and fat content analysis.

a)



b)

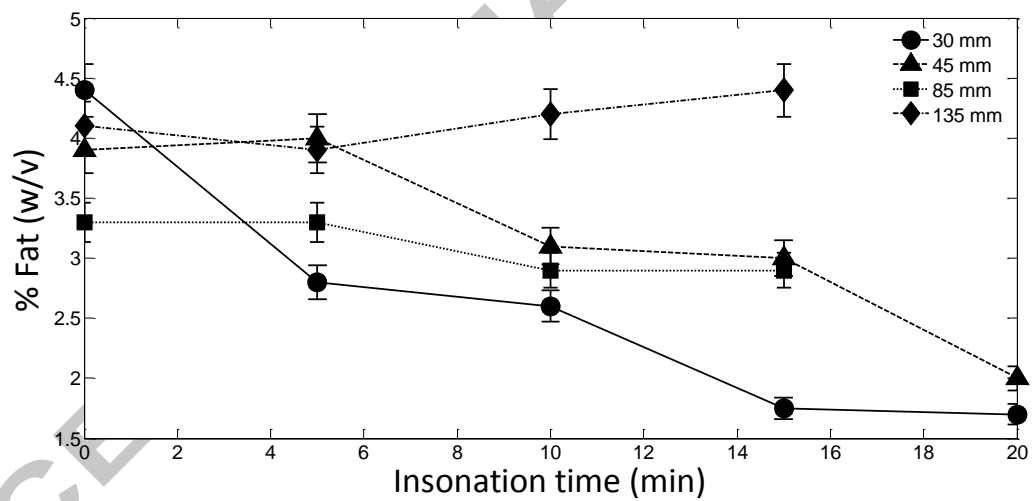


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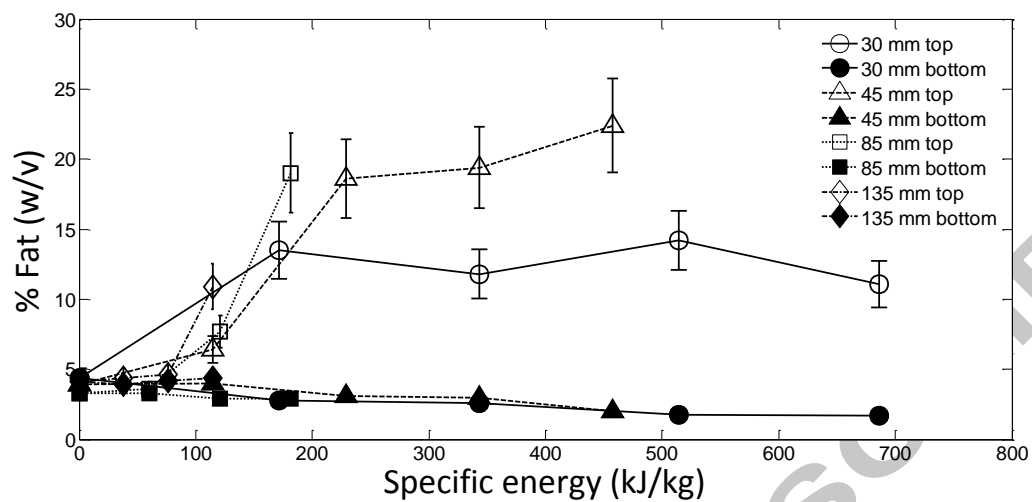


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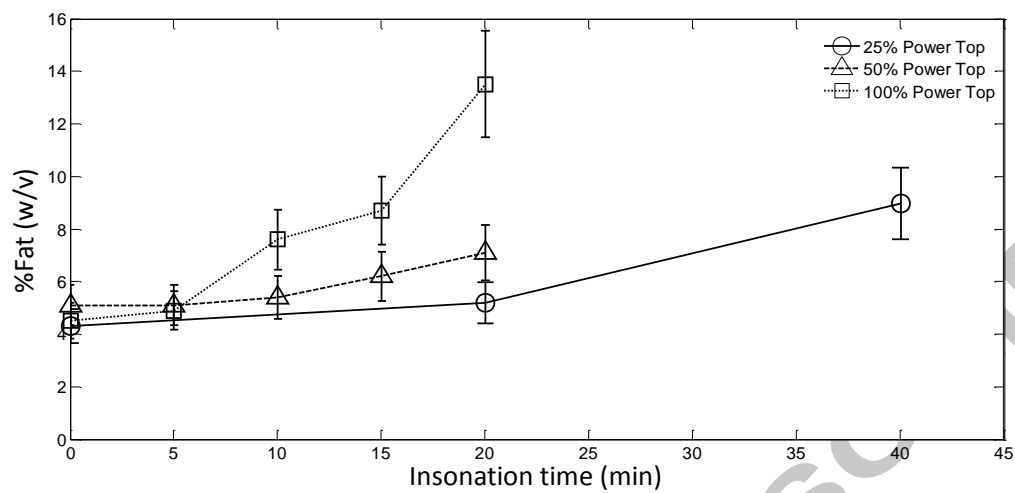


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Design parameters for the separation of fat from natural whole milk in an ultrasonic litre-scale vessel

Research Highlights

- ▶ Ultrasonic separation of milk fat from natural whole milk has been demonstrated only in millilitre scale systems previously
- ▶ Separation was enhanced in a litre scale ultrasonic reactor holding several transducer arrangements
- ▶ The duration of insonation, vessel dimensions, and specific energy input influenced separation
- ▶ Ultrasound application at parameters suitable for separation did not disrupt the integrity of fat globules
- ▶ This research identifies the key parameters to develop an ultrasonic milk fat separation device